

### C-1-3 Optional Components

#### MCM Series

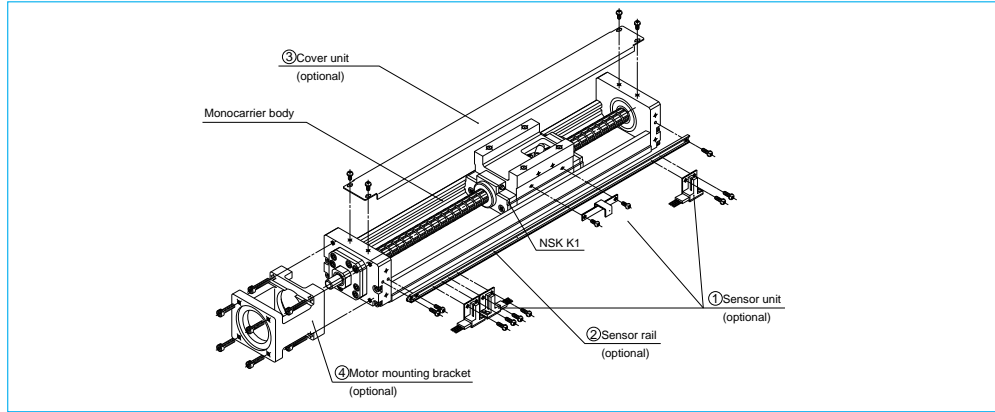


Fig. 3.1 Assembly Optional components for MCM10 (example)

- ① Sensor unit : Sensors, sensor mounting parts and a sensor dog are available in a set.  
\* When a sensor unit is used, the full cover unit cannot be used.
  - ② Sensor rail : Rail for sensor mounting is available.
  - ③ Cover unit : Top cover or full cover (included top cover and side cover) is available.
  - ④ Motor bracket for motor mounting : Available for a variety of models.
- Note: We assemble optional components upon request.

#### MCH Series

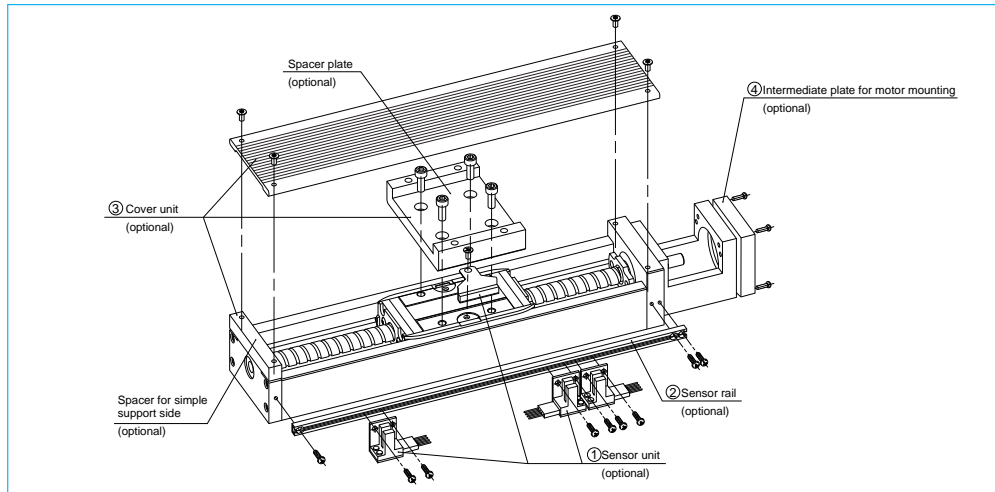


Fig. 3.2 Assembly Optional components for MCH10 (example)

- ① Sensor unit : Sensors, sensor mounting parts and a sensor dog are available in a set.
  - ② Sensor rail : Rail for sensor mounting is available.
  - ③ Cover unit : Top cover (included spacer plate and spacer for simple support side) is available.
  - ④ Intermediate plate for motor mounting : Available for a variety of models.
- Note: We assemble optional components upon request.

### C-1-4 Selection of Monocarrier

#### C-1-4. 1 Procedures for Selecting Monocarrier

Select a reference type of Monocarrier based on stroke and rigidity (Refer to Fig. 4.2, 4.3).

Select a ball screw lead referring to "C-1-4.3 Maximum Speed" so that the rotational speed does not exceed the limit.

Study the loads to be applied to the linear guide and obtain the equivalent load ( $F_e$ ) substituting them for equation ① or ② on Page C13. Obtain the mean effective load ( $F_m$ ) substituting them for equation ③ on Page C14, then calculate the life.

Study the loads to be applied to the ball screw and support unit. Obtain the mean effective load ( $F_m$ ) substituting them for equation ③ on Page C14, then calculate the life.

#### C-1-4. 2 Rigidity

##### Rigidity of rail

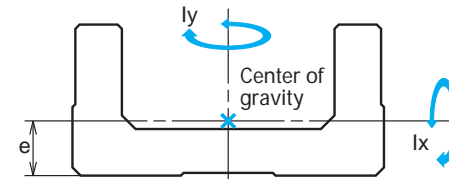


Fig. 4.1

Table 4.1 Rigidity of rail

Nominal size	Geometrical moment of inertia $\times 10^4$ (mm <sup>4</sup> )		Center of gravity (mm)	Mass (kg/100mm)
	$I_x$	$I_y$	$e$	$w$
MCM02	0.097	1.32	3.3	0.11
MCM03	0.30	3.3	4.5	0.18
MCM05	0.78	11.4	6.0	0.31
MCM06	2.14	26.1	7.0	0.57
MCM08	5.90	81.0	9.2	0.88
MCM10	15.6	219	12.2	1.52
MCH06	6.5	38.2	10.8	0.67
MCL06	2.58	29.6	7.8	0.56
MCH09	28.7	172	15.5	1.48
MCH10	54.0	307	18	1.93

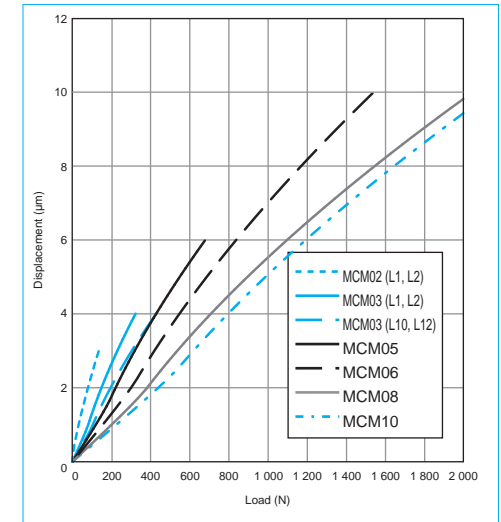


Fig. 4.2 MCM Series Rigidity in radial direction

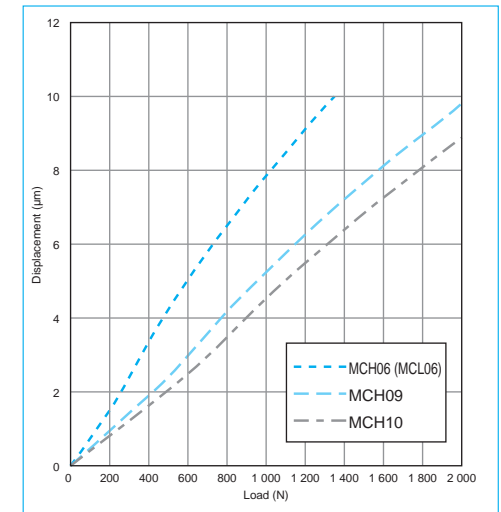


Fig. 4.3 MCH Series Rigidity in radial direction

C-1-4. 3 Maximum Speed

(1) Maximum Speed of MCM Series

Maximum speed of the Monocarrier is determined by the critical speed of the ball screw shaft and the  $d \cdot n$  value. Do not exceed the maximum speeds on the table below.

Table 4.2

	Ball screw lead	stroke (mm)	Rail length L <sub>2</sub> (mm)	Maximum speed (mm/s)
MCM02 Single slider	1	50	100	50
		100	150	
		150	200	
	2	50	100	100
		100	150	
		150	200	
MCM03 Single slider	1	50	115	50
		100	190	
		150	240	
	2	50	115	100
		100	190	
		150	240	
	10	100	190	500
		250	340	
		100	190	
12	100	190	600	
	250	340		
	50	180		
MCM05 Single slider	5	200	330	250
		50	180	
	10	600	730	500
		300	430	
	20	600	730	1000
		60	280	
MCM05 Double slider	10	510	730	500
		210	430	
		510	730	
	20	510	730	1000
		50	190	
		500	640	
MCM06 Single slider	5	50	190	250
		600	740	
		700	840	
		800	940	
	10	300	440	500
		600	740	
		700	840	
		800	940	
		800	940	
MCM06 Double slider	5	110	340	250
		410	640	
		110	340	
	10	610	840	500
		710	940	
		210	440	
20	610	840	1000	
	710	940		
	710	940		

Note: When operating the Monocarriers near the critical speed or exceeding the maximum speed in the table, please consult NSK.

	Ball screw lead	stroke (mm)	Rail length L <sub>2</sub> (mm)	Maximum speed (mm/s)
MCM08 Single slider	5	50	220	250
		200	370	
		100	270	
	10	700	870	500
		800	970	
		300	470	
20	700	870	1000	
	800	970		
	80	370		
MCM08 Double slider	10	680	970	500
		180	470	
		680	970	
	20	680	970	1000
		200	380	
		800	980	
MCM10 Single slider	10	900	1080	440
		1000	1180	
		300	480	
	20	800	980	1000
		900	1080	
		1000	1180	
MCM10 Double slider	10	70	380	500
		670	980	
		870	1180	
	20	170	480	1000
		670	980	
		870	1180	

Note: When operating the Monocarriers near the critical speed or exceeding the maximum speed in the table, please consult NSK.

(2) Maximum Speed of MCH Series

Maximum speed of the Monocarrier is determined by the critical speed of the ball screw shaft and the  $d \cdot n$  value. Do not exceed the maximum speeds on the table below.

Table 4.3

	Ball screw lead	stroke (mm)	Rail length L <sub>2</sub> (mm)	Maximum speed (mm/s)
MCH06 MCL06 Single slider	5	50	150	250
		500	600	
		50	150	
	10	500	600	500
		50	150	
		500	600	
20	50	150	1000	
	500	600		
	100	300		
MCH06 Double slider	5	400	600	250
		100	300	
		400	600	
	10	100	300	500
		400	600	
		100	300	
20	100	300	1000	
	400	600		
	200	340		
MCH09 Single slider	5	600	740	250
		800	940	
		200	340	
	10	600	740	500
		800	940	
		200	340	
MCH09 Double slider	5	150	440	250
		650	940	
		150	440	
	10	150	440	500
		650	940	
		150	440	
20	150	440	1000	
	650	940		
	650	940		

Note: When operating the Monocarriers near the critical speed or exceeding the maximum speed in the table, please consult NSK.

	Ball screw lead	stroke (mm)	Rail length L <sub>2</sub> (mm)	Maximum speed (mm/s)
MCH10 Single slider	10	400	580	500
		900	1080	
		800	980	
		900	1080	
		1000	1180	
		1100	1280	
	20	1200	1380	1000
		400	580	
		800	980	
		900	1080	
MCH10 Double slider	10	1000	1180	360
		1100	1280	
		1200	1380	
		400	580	
		800	980	
		900	1080	
	20	1000	1180	720
		1100	1280	
		1200	1380	
		250	580	
MCH10 Single slider	10	750	1080	480
		850	1180	
		950	1280	
		1050	1380	
		250	580	
		750	1080	
	20	850	1180	950
		950	1280	
		1050	1380	
		250	580	

Note: When operating the Monocarriers near the critical speed or exceeding the maximum speed in the table, please consult NSK.

C-1-4. 4 Accuracy Grade

The accuracy grade of Monocarrier standard inventories is high grade (H), except for lead 1 and 2 of MCM02, and 03.

When you require strokes longer than 1200 mm, please consult NSK about the accuracy grade.

Table 4.4 (Unit : μm)

Grade Stroke (mm)	High grade			Precision			
	Repeatability	Running Parallelism (vertical)	Backlash	Repeatability	Positioning accuracy	Running Parallelism (vertical)	Backlash
- 200	±10	14	20 or less	±3	20	8	3 or less
- 400		16			25	10	
- 600		20			30	12	
- 700		23			30	15	
- 1000		23			35	15	
- 1200		30			40	20	

C-1-4. 5 Stroke and Ball Screw Lead

(1) MCM Series Standard Combinations of Stroke and Ball Screw Lead

Table 4.5 Single slider (Unit : mm)

Nominal size lead stroke	MCM02		MCM03		MCM05			MCM06			MCM08			MCM10			
	1	2	1	2	10	12	5	10	20	5	10	20	5	10	20	10	20
50	○	○	○	○	☆	☆	○	○	☆	○	☆	☆	☆	☆			
100	○	○	○	○	○	○	○	○	☆	○	○	☆	☆	○	☆	☆	☆
150	○		☆	☆	☆	☆	☆	○	☆	☆	☆	☆	☆	☆	☆	☆	☆
200					○	☆	○	☆	○	☆	☆	☆	○	☆	○	☆	☆
250					☆	☆	☆	○	☆	☆	☆	☆	☆	☆	☆	☆	☆
300							☆	○	○	○	○	☆	○	○	○	○	○
400							☆	○	○	○	○	☆	○	○	○	○	○
500							☆	○	○	☆	○	☆	○	○	☆	☆	☆
600							☆	○	○	☆	☆	☆	○	☆	○	☆	☆
700										☆	○	○	☆	☆	☆	☆	☆
800										☆	☆	☆	☆	☆	○	☆	☆
900																☆	☆
1000																☆	☆

Table 4.6 Double slider (Unit : mm)

Nominal size lead stroke	MCM05		MCM06			MCM08		MCM10	
	10	20	5	10	20	10	20	10	20
60	☆								
70									☆
80						☆			
110	☆		☆	☆					
160	☆								
170								☆	☆
180						☆	☆		
210	☆	☆	☆	☆	☆				
270								☆	☆
280						☆	☆		
310	☆	☆	☆	☆	☆				
370								☆	☆
380						☆	☆		
410	☆	☆	☆	☆	☆				
470								☆	☆
480						☆	☆		
510	☆	☆		☆	☆				
570								☆	☆
580						☆	☆		
610				☆	☆				
670								☆	☆
680						☆	☆		
710				☆	☆				
870								☆	☆

Note: Please consult NSK about double slider of MCM 02 and 03.

(2) MCH Series Standard Combinations of Stroke and Ball Screw Lead

Table 4.7 Single slider

(○mark, Standard inventory; ☆mark, Short-term delivery) (Unit : mm)

Nominal size lead stroke	MCH06			MCH09			MCH10	
	5	10	20	5	10	20	10	20
50	○	○	☆					
100	○	○	☆	☆	☆	☆	☆	☆
200	○	○	○	○	○	☆	☆	☆
300	☆	○	○	○	○	☆	☆	☆
400	☆	○	○	○	○	☆	○	○
500	☆	○	○	☆	○	○	○	○
600				☆	○	○	○	○
700				☆	☆	☆	○	○
800				☆	○	○	○	○
900							☆	○
1000							☆	○
1100							☆	☆
1200							☆	☆

Table 4.8 Double slider

(☆mark, Short-term delivery) (Unit : mm)

Nominal size lead stroke	MCH06			MCH09			MCH10	
	5	10	20	5	10	20	10	20
100	☆	☆						
150				☆	☆			
200	☆	☆						
250				☆	☆		☆	☆
300	☆	☆						
350				☆	☆		☆	☆
400		☆	☆					
450					☆	☆	☆	☆
550							☆	☆
650					☆	☆	☆	☆
750								☆
850								☆
950								☆
1050								☆

Table 4.9 Limitations

	Nominal size	lead (mm)	slider	stroke (mm)
MCM series	MCM02	1, 2	Single	150
		1, 2	Single	150
	MCM03	10, 12	Single	350
			Single	900
	MCM05	5, 10, 20	Double	810
			Single	1000
	MCM06	5, 10, 20	Double	910
			Single	1000
MCM08	5, 10, 20	Double	880	
		Single	1800	
MCM10	10, 20	Double	1670	
		Single	600	
MCH series	MCH06	5, 10, 20	Double	500
			Single	1000
	MCH09	5, 10, 20	Double	850
			Single	1800
MCH10	10, 20	Double	1650	
		Single	500	
MCL06	5, 10, 20	Single	500	

C-1-4. 6 Basic Load Rating

(1) MCM Series Basic Load Rating

Table 4.10 Basic Load Rating

Nominal size	Lead $\ell$ (mm)	Shaft dia $d$ (mm)	Basic dynamic load rating (N)				Basic static load rating (N)		Support unit Limit load (N)
			Ball screw $C_a$	Linear guide $C$	Support unit $C_a$	Rated running distance $L_a$ (km)	Ball screw $C_{0a}$	Linear guide $C_0$	
MCM02	1	$\phi 6$	340 (High grade) 405 (Precision)	4910	615	1	555 (High grade) 615 (Precision)	2120	490
	2		340 (High grade) 405 (Precision)	3900		2	555 (High grade) 615 (Precision)		
MCM03	1	$\phi 6$	735	10900	2670	1	1230	4900	1040
	2		735	8650		2			
	10	1230	6250	10		1690			
	12	1230	5880	12					
MCM05	5	$\phi 12$	3760	15600	4400	5	6310	10900	1450
	10		2260	12400		10	3780		
	20		2260	9850		20	3780		
MCM06	5	$\phi 16$	7310	25200	6550	5	13500	17000	2730
	10		7060	20000		10	12700		
	20		4560	15900		20	7750		
MCM08	5	$\phi 16$	7310	30800	7100	5	13500	22800	3040
	10		7060	24400		10	12700		
	20		4560	19400		20	7750		
MCM10	10	$\phi 20$	10900	33500	7600	10	21700	29400	3380
	10		10900	33500		10	21700		
	20		7060	26600		20	12700		

Notes: ● Basic dynamic and static load ratings indicate the values for one slider. ● Basic dynamic load rating of the linear guide is the load of perpendicular direction to the axis that allows 90% of a group of the same Monocarriers to operate "Rated running distance" in the table, that is equivalent to 1 million revolutions of the ball screw and the support unit, under the same condition without causing flaking by rolling contact fatigue. ● Basic dynamic load rating of the ball screw is a load to axial direction that allows 90% of ball screws of a group of the same Monocarriers to rotate 1 million revolutions under the same condition without causing flaking by rolling contact fatigue. ● Basic dynamic load rating of the support unit is a constant load to axial direction that allows 90% of support units of the same group of Monocarriers to rotate 1 million revolutions under the same condition without causing flaking by rolling contact fatigue. ● Basic static load rating is a load that results in combined permanent deformations at the contact points of balls and ball grooves of respective parts is 0.01% of the diameter.

Table 4.11 Basic static moment load of linear guide

Nominal size	Lead (mm)	Slider	Basic static moment (N · m)		
			Rolling $M_{RO}$	Pitching $M_{PO}$	Yawing $M_{YO}$
MCM02	1, 2	Single	24	8	8
			MCM03	1, 2	68
10, 12	92				51
	MCM05		5, 10, 20	229	89
455				765	765
MCM06	5, 10, 20		415	174	174
		825	1220	1220	
MCM08	5, 10, 20	770	300	300	
		1540	2050	2050	
MCM10	10, 20	1170	425	425	
		2340	2940	2940	

Notes: ● Basic static moment of double slider is a value when two sliders equipped with NSK K1 are butted against each other. ● The basic static moment is the value when a rolling contact pressure of balls exceeds 4000 N/mm<sup>2</sup>. ● If you plan to apply extremely heavy load, please consult NSK for estimation of fatigue life.

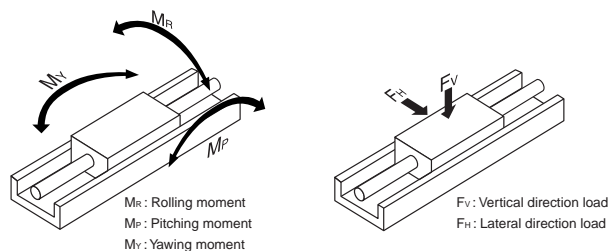


Fig. 4.4

(2) MCH Series Basic Load Rating

Table 4.12 Basic Load Rating

Nominal size	Lead $\ell$ (mm)	Shaft dia $d$ (mm)	Basic dynamic load rating (N)				Basic static load rating (N)		Support unit Limit load (N)
			Ball screw $C_a$	Linear guide $C$	Support unit $C_a$	Rated running distance $L_a$ (km)	Ball screw $C_{0a}$	Linear guide $C_0$	
MCH06 (MCL06)	5	$\phi 12$	3000 (High grade) 3760 (Precision)	22800	4400	5	5410 (High grade) 6310 (Precision)	16300	1450
	10		1930 (High grade) 2260 (Precision)	18100		10	3160 (High grade) 3780 (Precision)		
	20		1930 (High grade) 2260 (Precision)	14400		20	3160 (High grade) 3780 (Precision)		
MCH09	5	$\phi 15$	6820 (High grade) 7100 (Precision)	40600	7100	5	13200 (High grade) 13000 (Precision)	30500	3040
	10		5110 (High grade) 7060 (Precision)	32200		10	9290 (High grade) 12700 (Precision)		
	20		3290 (High grade) 4560 (Precision)	25500		20	5620 (High grade) 7750 (Precision)		
MCH10	10	$\phi 20$	8230 (High grade) 10900 (Precision)	44600	7600	10	17100 (High grade) 21700 (Precision)	42000	3380
	10		5300 (High grade) 7060 (Precision)	35400		10	10300 (High grade) 12700 (Precision)		
	20		7060 (Precision)	35400		20	12700 (Precision)		

Notes: ● Basic dynamic and static load ratings indicate the values for one slider. ● Basic dynamic load rating of the linear guide is the load of perpendicular direction to the axis that allows 90% of a group of the same Monocarriers to operate "Rated running distance" in the table, that is equivalent to 1 million revolutions of the ball screw and the support unit, under the same condition without causing flaking by rolling contact fatigue. ● Basic dynamic load rating of the ball screw is a load to axial direction that allows 90% of ball screws of a group of the same Monocarriers to rotate 1 million revolutions under the same condition without causing flaking by rolling contact fatigue. ● Basic dynamic load rating of the support unit is a constant load to axial direction that allows 90% of support units of the same group of Monocarriers to rotate 1 million revolutions under the same condition without causing flaking by rolling contact fatigue. ● Basic static load rating is a load that results in combined permanent deformations at the contact points of balls and ball grooves of respective parts is 0.01% of the diameter.

Table 4.13 Basic static moment load of linear guide

Nominal size	Slider	Basic static moment (N · m)		
		Rolling $M_{RO}$	Pitching $M_{PO}$	Yawing $M_{YO}$
MCH06 (MCL06)	Single	335	133	133
	Double	770	730	730
MCH09	Single	890	385	385
	Double	1780	2070	2070
MCH10	Single	1460	610	610
	Double	2920	3430	3430

Notes: ● Basic static moment of double slider is a value when two sliders equipped with NSK K1 are butted against each other. ● The basic static moment is the value when a rolling contact pressure of balls exceeds 4000 N/mm<sup>2</sup>. ● If you plan to apply extremely heavy load, please consult NSK for estimation of fatigue life.

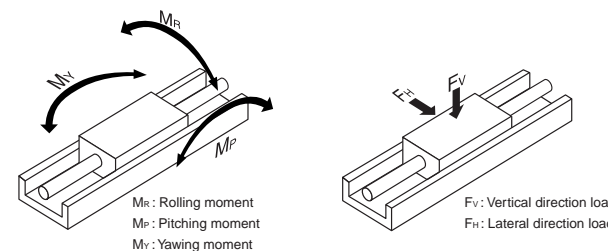


Fig. 4.5

C-1-4. 7 Estimation of Life Expectancy

(1) Life of Linear Guide

Study the load to be applied to the linear guide of Monocarrier (Fig. 4.6). The equivalent load (Fe) is determined by substituting the load for equation ① (Eq.② : in case of the tightly coupled double slider type).

● In case of the single slider

$$F_e = Y_H F_H + Y_V F_V + Y_R \epsilon_{Rd} M_R + Y_P \epsilon_{Pd} M_P + Y_Y \epsilon_{Yd} M_Y \dots ①$$

● In case of the double slider

$$F_e = \frac{Y_H F_H}{2} + \frac{Y_V F_V}{2} + Y_R \epsilon_{Rd} M_R + Y_P \epsilon_{Pd} M_P + Y_Y \epsilon_{Yd} M_Y \dots ②$$

- F<sub>H</sub> : Lateral direction load acting on the slider (N)
- F<sub>V</sub> : Vertical direction load acting on the slider (N)
- M<sub>R</sub> : Rolling moment acting on the slider (N · m)
- M<sub>P</sub> : Pitching moment acting on the slider (N · m)
- M<sub>Y</sub> : Yawing moment acting on the slider (N · m)

- ε<sub>Rd</sub> ε<sub>Rd</sub> : Dynamic equivalent coefficient to rolling moment
- ε<sub>Pd</sub> ε<sub>Pd</sub> : Dynamic equivalent coefficient to pitching moment
- ε<sub>Yd</sub> ε<sub>Yd</sub> : Dynamic equivalent coefficient to yawing moment

Refer to Table 4.14 about Dynamic equivalent coefficient.

- Y<sub>H</sub>, Y<sub>V</sub>, Y<sub>R</sub>, Y<sub>P</sub>, Y<sub>Y</sub> : 1.0 or 0.5

At equations ① and ② for obtaining equivalent load Fe, among F<sub>H</sub>, F<sub>V</sub>, ε<sub>Pd</sub>M<sub>P</sub>, ε<sub>Rd</sub>M<sub>R</sub>, ε<sub>Yd</sub>M<sub>Y</sub>, the maximum load is assumed to be 1.0, and others are to be 0.5.

Table 4.14 Dynamic equivalent coefficient

Nominal size	MCM02	MCM03		MCM05	MCM06	MCM08	MCM10	MCH06 MCL06	MCH09	MCH10
		lead 1, 2	lead 10, 12							
ε <sub>R</sub>	95.2	79.4	79.4	52.6	45.5	32.5	27.8	48.3	34.5	28.6
ε <sub>P</sub>	174	113.9	84.2	81.3	65.1	48.8	45.2	75.1	47.9	41.0
ε <sub>Y</sub>	174	113.9	84.2	81.3	65.1	48.8	45.2	75.1	47.9	41.0
ε <sub>Rd</sub>	-	-	-	26.3	22.7	16.3	13.9	24.2	17.2	14.3
ε <sub>Pd</sub>	-	-	-	10.4 (12.2)	9.7 (11.5)	7.6 (8.6)	7.1 (8.0)	11.4 (13.2)	8.11 (9.10)	6.98 (7.82)
ε <sub>Yd</sub>	-	-	-	10.4 (12.2)	9.7 (11.5)	7.6 (8.6)	7.1 (8.0)	11.4 (13.2)	8.11 (9.10)	6.98 (7.82)

Note: Parenthesized figures are Dynamic equivalent coefficient in case of the Monocarrier without NSK K1.

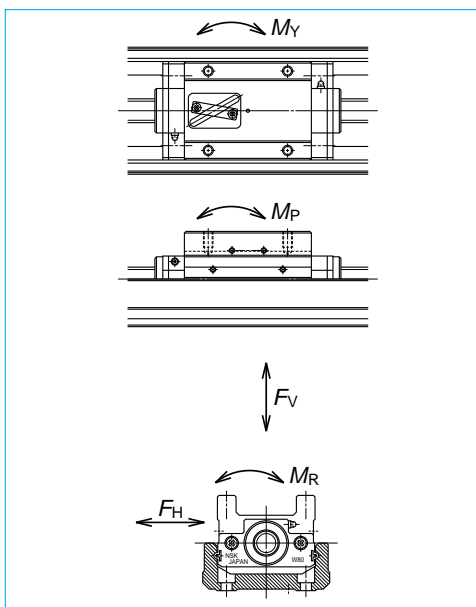


Fig. 4.6 Direction of load

In case when the load acting on the slider may fluctuate (In general, M<sub>p</sub>, M<sub>r</sub> may fluctuate with the acceleration/deceleration of slider), the mean effective load is determined by Eq. ③.

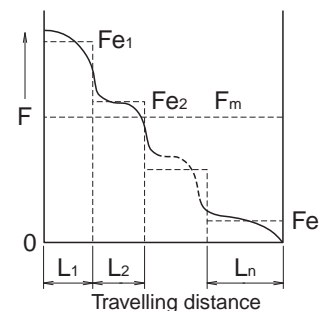


Fig. 4.7 Stepwise Fluctuating Load

Travelling distance under the equivalent load Fe<sub>1</sub> : L<sub>1</sub>  
 Travelling distance under the equivalent load Fe<sub>2</sub> : L<sub>2</sub>  
 . . . . .  
 Travelling distance under the equivalent load Fe<sub>n</sub> : L<sub>n</sub>

$$F_m = \sqrt[3]{\frac{1}{L} (F_{e1}^3 L_1 + F_{e2}^3 L_2 + \dots + F_{en}^3 L_n) \dots ③}$$

F<sub>m</sub> : Mean effective load of fluctuating loads  
 L : Total travelling distance

The life of linear guide is calculated by Eq. ④

$$L = L_a \times \left( \frac{C}{f_w \cdot F_m} \right)^3 \dots ④$$

- L : Life of linear guide (km)
- F<sub>m</sub> : Mean effective load acting on the linear guide (N)
- C : Basic dynamic load rating of the linear guide (N)
- L<sub>a</sub> : Travelling distance (km)
- f<sub>w</sub> : Load factor (Refer to Table 4.15)

When the estimated life does not clear the required life, the life of the linear guide is to be calculated again after the following measures are taken:

1. Change from the single slider type to double slider type.
2. Use a larger size Monocarrier.

(2) Life of Ball Screw (Support unit)

The mean effective load is determined from the axial loads.

For calculation of the mean effective load, use Eq.③.

The life of ball screw is calculated by Eq. ⑤.

$$L = \ell \times \left( \frac{C_a}{f_w \cdot F_m} \right)^3 \times 10^6 \dots ⑤$$

- ℓ : Lead of ball screw (mm)
- L : Life of ball screw (mm)
- C<sub>a</sub> : Basic dynamic load rating of the ball screw (N)
- F<sub>m</sub> : Mean effective load acting on the ball screw (N)
- f<sub>w</sub> : Load factor (Refer to Table 4.15)

The life of a support unit is calculated by Eq. ⑤. If the life of ball screw / support unit does not clear the required life, use a larger size Monocarrier. After applying the calculations mentioned above, selection of the Monocarrier is completed.

Table 4.15 Values of load factor f<sub>w</sub>

Operating conditions	Load factor f <sub>w</sub>
At smooth operation with no mechanical shock	1.0 – 1.2
At normal operation	1.2 – 1.5
At operation with mechanical shock and vibrations	1.5 – 3.0

C-1-4. 8 Example of Life Estimation

This section offers an example how to estimate the life of Monocarrier based on the life of each component.

<<Example of calculation-1>>

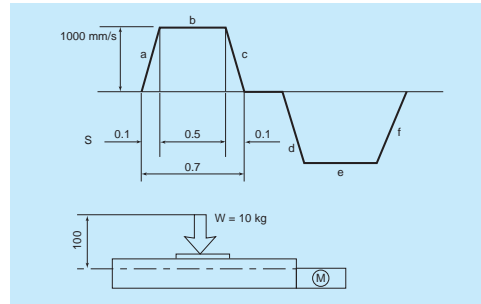


Fig. 4.8

1. Use condition

- Stroke : 600 mm
- Maximum Speed : 1000 mm/s
- Load Mass : W = 10 kg
- Acceleration : g = 9.8 m/s<sup>2</sup>
- Setting Position : Horizontal
- Operating Profile : See above figure

2. Selection of Nominal size (Interim Selection)

Firstly, select a greater ball screw lead as the maximum speed is 1000 mm/s. The interim selection is MCM06060H20K00, a single slider specification MCM06 that has 600 mm stroke, as the stroke is 600 mm.

3. Calculation

3-1. Linear guide

3-1-1. Fatigue life

Multiply the result of the Eq. ① by the dynamic equivalent coefficient (Table 4.14 single slider) to convert the load volume. From above operation profile,

- i) Constant speed  $Fe_1 = Y_V F_V = Y_V W g = 1 \cdot 10 \cdot 9.8 = 98 \text{ N}$
- ii) Accelerating  $Fe_2 = Y_V F_V + Y_P \epsilon_P M_p = 0.5 \cdot 10 \cdot 9.8 + 1 \cdot 65.1 \cdot 0.1 \cdot 100 = 700 \text{ N}$
- iii) Decelerating  $Fe_3 = Y_V F_V + Y_P \epsilon_P M_p = 0.5 \cdot 10 \cdot 9.8 + 1 \cdot 65.1 \cdot 0.1 \cdot 100 = 700 \text{ N}$

Mean effective load  $F_m$

$$F_m = \sqrt[3]{\frac{1}{L} (Fe_1^3 \cdot L_1 + Fe_2^3 \cdot L_2 + Fe_3^3 \cdot L_3)}$$

$$= \sqrt[3]{\frac{1}{600} (98^3 \cdot 500 + 700^3 \cdot 50 + 700^3 \cdot 50)}$$

$$= 387 \text{ N}$$

$$L = \left( \frac{C}{f_w \cdot F_m} \right)^3 \times L_a$$

$$= \left( \frac{15900}{1.2 \cdot 387} \right)^3 \times 20$$

$$= 8.02 \times 10^5 \text{ km}$$

3-1-2. Static safety factor; Divide the basic static load rating by the maximum load.

$$F_s = \frac{C_0}{F_e} = \frac{C_0}{F_{e2}} = \frac{17000}{700} = 24.2$$

3-2. Ball screw

3-2-1. Fatigue life; Obtain the axial load of each stage of operation referring to the operation profile, then calculate the mean load.

By the process above,

- i) Constant speed  $Fe_1 = \mu \cdot W \cdot g = 0.01 \cdot 10 \cdot 9.8 = 0.98$
- ii) Accelerating  $Fe_2 = Fe_1 + W\alpha = 101 \text{ N}$
- iii) Decelerating  $Fe_3 = Fe_1 - W\alpha = 99 \text{ N}$

Axial mean effective load  $F_m$

$$F_m = \sqrt[3]{\frac{1}{L} (Fe_1^3 \cdot L_1 + Fe_2^3 \cdot L_2 + Fe_3^3 \cdot L_3)}$$

$$= \sqrt[3]{\frac{1}{600} (0.98^3 \cdot 500 + 101^3 \cdot 50 + 99^3 \cdot 50)}$$

$$= 55 \text{ N}$$

$$L = \left( \frac{C_a}{f_w \cdot F_m} \right)^3 \times \ell \times 10^6$$

$$= \left( \frac{4560}{1.2 \cdot 55} \right)^3 \times 20 \times 10^6 \text{ (mm)}$$

$$= 6.5 \times 10^6 \text{ km}$$

3-2-2. Static safety factor; Divide the basic static load rating by the maximum axial load.

$$F_s = \frac{C_{0a}}{F_e} = \frac{C_{0a}}{F_{e2}} = \frac{7750}{101} = 76.7$$

3-2-3. Maximum rotational speed; According to the table of maximum speed on page C7, MCM06 with 20 mm lead and 600 mm stroke, is possible to operate under the maximum speed of 1000 mm/s.

3-3. Support unit

3-3-1. Fatigue life; Use the axial load  $F_m = 55 \text{ N}$ , that is the result of above calculation 3-2-1.

$$L = \left( \frac{C_a}{f_w \cdot F_m} \right)^3 \times \ell \times 10^6 = \left( \frac{6550}{1.2 \times 55} \right)^3 \times 20 \times 10^6 \text{ (mm)}$$

$$= 1.95 \times 10^7 \text{ km}$$

3-3-2. Static safety factor; Divide the limit load by the maximum axial load.

$$F_s = \frac{C_{0a}}{F_e} = \frac{C_{0a}}{F_{e2}} = \frac{2730}{101} = 27.0$$

3-4. Result

MCM06060H20K00	Linear guide	Ball screw	Support unit
Fatigue life	8.02 × 10 <sup>5</sup> km	6.5 × 10 <sup>6</sup> km	1.95 × 10 <sup>7</sup> km
Static safety factor	24.2	76.7	27.0

In this case, the linear guide has the shortest fatigue life of the components. Therefore, the linear guide fatigue life is used as the life of the Monocarrier. The interim selection of MCM06060H20K00, that is chosen based on the use conditions, satisfies the required life.

<<Example of calculation-2>>

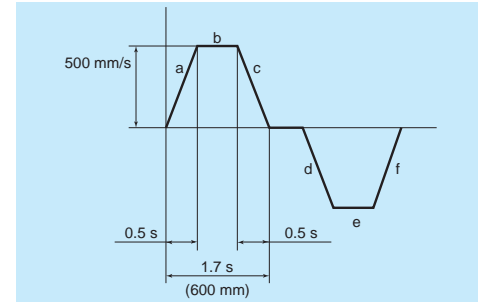


Fig. 4.9

1. Use condition

- Stroke : 600 mm
- Maximum Speed : 500 mm/s
- Load Mass : W = 20 kg
- Acceleration : 9.8 m/s<sup>2</sup>
- Setting Position : Vertical
- Operating Profile : See above figure

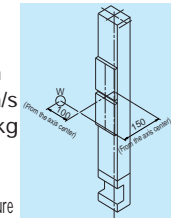


Fig. 4.10

2. Selection of Nominal size (Interim Selection)  
Select a 10 mm lead ball screw as the maximum speed is 500 mm/s.

The interim selection is MCM08068H10D00 as a double slider specification of MCM08 has 680 mm stroke, and the setting position is vertical.

3. Calculation

3-1. Linear guide

3-1-1. Fatigue life; Multiply the result of the Eq. ② by the dynamic equivalent coefficient (Table 4.14. double slider) to convert the load volume. From operation profile (Fig. 4.9), the acceleration is 1 m/s<sup>2</sup>.

- i) Constant speed  $Fe_1 = Y_p \times \epsilon_{pd} \times M_p + Y_v \times \epsilon_{vd} \times M_v$   
 $= 1 \cdot 7.6 \cdot 20 \cdot 9.8 \cdot 0.15 + 0.5 \cdot 7.6 \cdot 20 \cdot 9.8 \cdot 0.1 = 298 \text{ N}$
- ii) Accelerating  $Fe_2 = Y_p \times \epsilon_{pd} \times M_p + Y_v \times \epsilon_{vd} \times M_v$   
 $= 1 \cdot 7.6 \cdot 20 \cdot (9.8 + 0.15) \cdot 0.15 + 0.5 \cdot 7.6 \cdot 20 \cdot (9.8 + 1.0) \cdot 0.1 = 329 \text{ N}$
- iii) Decelerating  $Fe_3 = Y_p \times \epsilon_{pd} \times M_p + Y_v \times \epsilon_{vd} \times M_v$   
 $= 1 \cdot 7.6 \cdot 20 \cdot (9.8 - 1.0) \cdot 0.15 + 0.5 \cdot 7.6 \cdot 20 \cdot (9.8 - 1.0) \cdot 0.1 = 268 \text{ N}$

Mean effective load  $F_m$

$$F_m = \sqrt[3]{\frac{1}{L} (Fe_1^3 \cdot L_1 + Fe_2^3 \cdot L_2 + Fe_3^3 \cdot L_3)}$$

$$= \sqrt[3]{\frac{1}{600} (298^3 \cdot 350 + 329^3 \cdot 125 + 268^3 \cdot 125)}$$

$$= 300 \text{ N}$$

$$L = L_a \times \left( \frac{C}{f_w \cdot F_m} \right)^3$$

$$= 10 \times \left( \frac{24400}{1.2 \cdot 300} \right)^3$$

$$= 3.11 \times 10^6 \text{ km}$$

3-1-2. Static safety factor; Divide the basic static load rating by the maximum load.

$$F_s = \frac{C_0}{F_e} = \frac{C_0}{F_{e2}} = \frac{22800}{329} = 69.3$$

3-2. Ball screw

3-2-1. Fatigue life; Obtain the axial load of each stage of operation referring to the operation profile, then calculate the mean load.

- i) Constant speed  $Fe_1 = W \cdot g = 20 \cdot 9.8 = 196 \text{ N}$
- ii) Accelerating  $Fe_2 = Fe_1 + W \cdot \alpha = 196 + 20 \cdot 1 = 216 \text{ N}$
- iii) Decelerating  $Fe_3 = Fe_1 - W \cdot \alpha = 196 - 20 \cdot 1 = 176 \text{ N}$